

332:345 – Linear Systems & Signals – Fall 2009
Sample Final Exam Questions

- Please review all sample questions for exams 1 & 2.
- Consider a second-order analog audio parametric equalizer filter,

$$H(s) = \frac{G\alpha s + G_0(s^2 + \omega_0^2)}{s^2 + \alpha s + \omega_0^2}, \quad \alpha = \sqrt{\frac{G_B^2 - G_0^2}{G^2 - G_B^2}} \Delta\omega \quad (1)$$

where G, G_0, G_B are the peak, reference, and bandwidth gains, and $\Delta\omega$ is the bandwidth measured at level G_B .

- Often the bandwidth gain is defined to be the geometric mean of the peak and reference gains, that is, $G_B = (GG_0)^{1/2}$. Show that this choice corresponds to the arithmetic mean of the gains in dB units. (The dB gains are defined by $G_{dB} = 20 \log_{10}(G)$, etc.)
- Set $G_0 = 1$. For the above geometric-mean choice for G_B , show that an equalizer of boost gain G_{dB} at center frequency ω_0 and width $\Delta\omega$, is the exact inverse of an equalizer with a cut gain by an equal amount $-G_{dB}$ at the same center frequency and width, i.e., show that the corresponding boost and cut transfer functions will be related by,

$$H_{\text{boost}}(s)H_{\text{cut}}(s) = 1$$

- Set $G_0 = 1$. For the above geometric-mean choice for G_B , show that the equalizer corresponding to peak gain G and center frequency ω_0 and width $\Delta\omega$ is given by:

$$H(s) = \frac{s^2 + \Delta\omega G^{1/2}s + \omega_0^2}{s^2 + \Delta\omega G^{-1/2}s + \omega_0^2}$$

You may use this result to prove part(b).

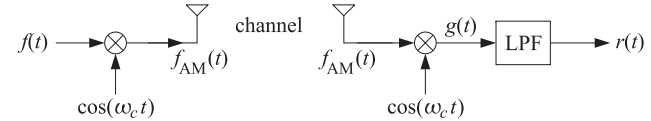
- Consider again the more general version of the equalizer given by Eq. (1). In audio work the bandwidth is usually expressed in octaves, that is, a bandwidth of say B octaves means that the ratio of the upper and lower bandedge frequencies is given by

$$\frac{\omega_2}{\omega_1} = 2^B \Rightarrow B = \log_2 \left(\frac{\omega_2}{\omega_1} \right) = \text{octave bandwidth}$$

Using the fact that $\omega_2\omega_1 = \omega_0^2$, show that the actual bandwidth $\Delta\omega$ in units of rads/sec is related to the octave bandwidth B by

$$\Delta\omega = 2\omega_0 \sinh \left(\frac{1}{2} B \ln(2) \right)$$

- The transmitter and receiver of an AM communication system are depicted below. The baseband signal to be transmitted is $f(t)$ and has Fourier transform $F(\omega)$ assumed to be bandlimited in the interval $|\omega| \leq \omega_B$.



The modulated transmitted signal and its demodulated version at the receiver will be:

$$f_{AM}(t) = \cos(\omega_c t) f(t)$$

$$g(t) = \cos(\omega_c t) f_{AM}(t)$$

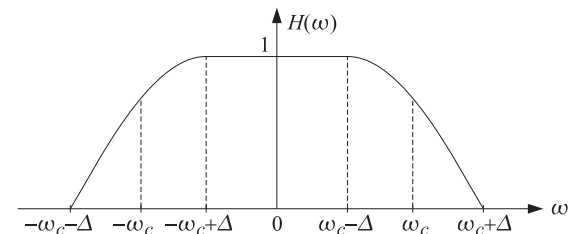
- Express the spectra of $f_{AM}(t)$ and $g(t)$ in terms of the original spectrum $F(\omega)$ and make a rough sketch of them versus ω , assuming that $\omega_c \gg \omega_B$.
- Discuss the need for the indicated lowpass filter (LPF) and explain how to pick its specifications.
- Explain why the above system would fail if the receive-carrier $\cos(\omega_c t)$ were to be replaced by $\sin(\omega_c t)$, i.e., $g(t) = \sin(\omega_c t) f_{AM}(t)$, having a 90° phase difference compared to the transmit-carrier. (In practice, any possible phase offset in the carrier signals is compensated using a phase-locked loop.)

[Hint: trig identity $2 \cos(\alpha) \cos(\beta) = \cos(\alpha + \beta) + \cos(\alpha - \beta)$.]

- The square-root raised-cosine filter is probably the most widely used pulse shaping filter in digital communication systems. Its frequency response is bandlimited and is defined by,

$$P(\omega) = \begin{cases} 1, & |\omega| \leq \omega_c - \Delta \\ \cos \left(\frac{\pi}{4\Delta} (|\omega| - \omega_c + \Delta) \right), & \omega_c - \Delta \leq |\omega| \leq \omega_c + \Delta \\ 0, & |\omega| > \omega_c + \Delta \end{cases}$$

where $\Delta < \omega_c$. It has a flat response over the interval $|\omega| \leq \omega_c - \Delta$, and beyond that, it tapers to zero following a cosine curve. It is depicted below.



- (a) Verify that $P(\omega)$ is the square root of the raised-cosine filter defined in the sample problems for exam-2.
- (b) By direct calculation of the inverse Fourier transform, show that the impulse response of this filter is given by,

$$p(t) = \frac{\sin((\omega_c - \Delta)t) + \frac{4t\Delta}{\pi} \cos((\omega_c + \Delta)t)}{\pi t \cdot \left[1 - \left(\frac{4t\Delta}{\pi}\right)^2\right]} \quad (2)$$

- (c) Show that its value at $t = 0$ is,

$$p(0) = \frac{\pi\omega_c + (4 - \pi)\Delta}{\pi^2}$$

and that its value at $t = \pm\pi/(4\Delta)$ is,

$$\frac{\sqrt{2}\Delta}{2\pi^2} \left[(\pi - 2) \cos\left(\frac{\pi\omega_c}{4\Delta}\right) + (\pi + 2) \sin\left(\frac{\pi\omega_c}{4\Delta}\right) \right]$$

- (d) To do the required Fourier integral for obtaining Eq. (2), first note that because $P(\omega)$ is even in ω , the integral simplifies into,

$$p(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} P(\omega) e^{j\omega t} d\omega = \frac{1}{\pi} \int_0^{\infty} P(\omega) \cos(\omega t) d\omega$$

Then, split the integral as follows,

$$p(t) = \frac{1}{\pi} \int_0^{\omega_c - \Delta} P(\omega) \cos(\omega t) d\omega + \frac{1}{\pi} \int_{\omega_c - \Delta}^{\omega_c + \Delta} P(\omega) \cos(\omega t) d\omega$$

Show that the first term is:

$$\frac{\sin((\omega_c - \Delta)t)}{\pi t}$$

and the second,

$$\frac{4\Delta}{\pi^2} \cdot \frac{\cos((\omega_c + \Delta)t) + \frac{4t\Delta}{\pi} \sin((\omega_c - \Delta)t)}{1 - \left(\frac{4t\Delta}{\pi}\right)^2}$$

Then, obtain Eq. (2) by adding up these two terms.

Hint: You may use the indefinite integral:

$$\int \cos(ax) \cos(bx) dx = \frac{\sin((a+b)x)}{2(a+b)} + \frac{\sin((a-b)x)}{2(a-b)}$$

5. Show that the inverse of an invertible 2×2 matrix is given explicitly as follows:

$$A = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \Rightarrow A^{-1} = \frac{1}{ad - bc} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$$

Then, show that its characteristic polynomial is given by

$$p(s) = \det(sI - A) = s^2 - \text{tr}(A)s + \det(A)$$

where I is the unit 2×2 matrix, and $\text{tr}(A)$, $\det(A)$ denote the trace and determinant of the matrix A . This is a general result for any 2×2 matrix.

Finally, verify the Cayley-Hamilton theorem by explicit matrix multiplication, that is, show that

$$p(A) = A^2 - \text{tr}(A)A + \det(A)I = 0$$

6. Consider the second-order linear system:

$$\ddot{y}(t) + a_1 \dot{y}(t) + a_2 y(t) = b_0 \ddot{f}(t) + b_1 \dot{f}(t) + b_2 f(t)$$

where the input $f(t)$ is assumed to be a causal function that does not have any impulsive terms (e.g., $\delta(t)$, $\dot{\delta}(t)$, etc.).

- (a) Show the following relationships between the output values at times $t = 0^-$ and $t = 0^+$:

$$\begin{aligned} y(0^+) - y(0^-) &= b_0 f(0^+) \\ \dot{y}(0^+) - \dot{y}(0^-) &= (b_1 - b_0 a_1) f(0^+) + b_0 \dot{f}(0^+) \end{aligned} \quad (3)$$

where because of the causality of $f(t)$, we used the result that $f(0^-) = \dot{f}(0^-) = 0$. Eqs. (3) allow one to map the initial conditions at 0^- to those at 0^+ . *Hint:* Integrate the differential equation once and then twice over the interval $[0^-, t]$ and then take the limit $t \rightarrow 0^+$:

$$\begin{aligned} \int_{0^-}^t [\ddot{y}(\tau) + a_1 \dot{y}(\tau) + a_2 y(\tau)] d\tau &= \int_{0^-}^t [b_0 \ddot{f}(\tau) + b_1 \dot{f}(\tau) + b_2 f(\tau)] d\tau \\ \int_{0^-}^t dt' \int_{0^-}^{t'} [\ddot{y}(\tau) + a_1 \dot{y}(\tau) + a_2 y(\tau)] d\tau &= \int_{0^-}^t dt' \int_{0^-}^{t'} [b_0 \ddot{f}(\tau) + b_1 \dot{f}(\tau) + b_2 f(\tau)] d\tau \end{aligned}$$

- (b) Consider the controller canonical state-space realization (actually, any other realization) of the above second-order system, and differentiate the output equation once to get the system:

$$\begin{aligned} \dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}f \\ y &= \mathbf{C}\mathbf{x} + Df \\ \dot{y} &= \mathbf{C}\dot{\mathbf{x}} + D\dot{f} = \mathbf{C}\mathbf{A}\mathbf{x} + \mathbf{C}\mathbf{B}f + D\dot{f} \end{aligned}$$

From the last two equations, argue that:

$$y(0+) - y(0-) = Df(0+)$$

$$\dot{y}(0+) - \dot{y}(0-) = CBf(0+) + D\dot{f}(0+)$$

and show that these are equivalent to Eqs. (3).

7. Consider an $[A, B, C, D]$ state-space representation of a single-input single-output (SISO) order- p system:

$$\dot{\mathbf{x}} = A\mathbf{x} + Bf$$

$$y = C\mathbf{x} + Df$$

where the state vector \mathbf{x} is a p -dimensional column vector. Given an arbitrary $p \times p$ invertible matrix V , define the transformed state vector $\mathbf{x}' = V\mathbf{x}$, and the transformed matrices:

$$A' = VAV^{-1}, \quad B' = VB, \quad C' = CV^{-1}, \quad D' = D$$

Show that these define a new state-space representation that satisfies:

$$\dot{\mathbf{x}}' = A'\mathbf{x}' + B'f$$

$$y = C'\mathbf{x}' + D'f$$

Moreover, show that $C'B' = CB$. How is this result relevant to the previous problem?

8. Consider the linear system described by the following second-order differential equation:

$$\ddot{y}(t) + 3\dot{y}(t) + 2y(t) = \ddot{f}(t) + f(t) \quad (4)$$

- (a) Find its transfer function $H(s)$ and draw the controller canonical realization form. *Answer:* $H(s) = \frac{s^2 + 1}{s^2 + 3s + 2}$.

- (b) Apply long-division to put $H(s)$ in the form,

$$H(s) = \frac{s^2 + 1}{s^2 + 3s + 2} = b_0 + \frac{c_1s + c_2}{s^2 + 3s + 2}$$

and determine the numerical values of the coefficients b_0, c_1, c_2 . Then draw the corresponding controller canonical realization form.

- (c) Applying the four transposition rules, draw the transposed realization of that of part (a), that is, the observer canonical form.

- (d) For the controller realization of part (a), define appropriate internal states and derive the corresponding $[A, B, C, D]$ state-space realization.

$$\text{Answers: } A = \begin{bmatrix} -3 & -2 \\ 1 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad C = [-3, -1], \quad D = 1.$$

- (e) Calculate the Laplace transform of the state transition matrix, i.e.,

$$\Phi(s) = (sI - A)^{-1}$$

where I is the 2×2 unit matrix. *Answer:* $\frac{1}{s^2 + 3s + 2} \begin{bmatrix} s & -2 \\ 1 & s + 3 \end{bmatrix}$.

- (f) By explicit matrix multiplication, calculate the system transfer function and show that it is correctly given by parts (a,b), that is, show that

$$H(s) = C(sI - A)^{-1}B + D$$

- (g) Perform a partial-fraction expansion on each entry of the matrix $\Phi(s)$ and then perform an inverse Laplace transform, thereby, obtaining the state transition matrix:

$$\phi(t) = e^{At}, \quad t \geq 0$$

$$\text{Answer: } \phi(t) = \begin{bmatrix} 2e^{-2t} - e^{-t} & 2e^{-2t} - 2e^{-t} \\ e^{-t} - e^{-2t} & 2e^{-t} - e^{-2t} \end{bmatrix}.$$

- (h) By explicit matrix multiplication, determine the impulse response of this system, that is,

$$h(t) = Ce^{At}B + D\delta(t) = C\phi(t)B + D\delta(t)$$

$$\text{Answer: } h(t) = (2e^{-t} - 5e^{-2t})u(t) + \delta(t).$$

- (i) Alternatively, obtain $h(t)$ by performing the inverse Laplace transform of $H(s)$ using partial-fraction expansions of part (b).
 (j) Next, assume that the input to Eq. (4) is $f(t) = e^{-3t}u(t)$. Using standard Laplace transform methods and partial-fraction expansions, solve Eq. (4) subject to arbitrary initial conditions, that is, arbitrary values for $y(0-)$ and $\dot{y}(0-)$. You should find the answer to be:

$$y(t) = (2y_0 + \dot{y}_0 + 1)e^{-t} - (y_0 + \dot{y}_0 + 5)e^{-2t} + 5e^{-3t} \quad (5)$$

for $t \geq 0$, where we used the shorthand notation $y_0 = y(0-)$ and $\dot{y}_0 = \dot{y}(0-)$.

- (k) Read sections 7.1, 7.4, 7.5, and 7.11 of your text on the issues that arise when the differential equation of the system contains time-derivatives of the input (which cause delta-function impulses). Using the techniques illustrated by Examples 7.5 and 7.21, solve part (j) by writing $y(t)$ as the sum of a homogeneous solution and a particular solution of the form:

$$y(t) = y_h(t) + y_p(t)$$

$$y_h(t) = Ae^{-t} + Be^{-2t}$$

$$y_p(t) = \int_{0-}^t h(t - \tau)f(\tau) d\tau$$

Fix A, B by imposing the initial conditions y_0, \dot{y}_0 . Verify that the resulting $y(t)$ is the same as that of Eq. (5). *Answers:*

$$y_h(t) = (2y_0 + \dot{y}_0)e^{-t} - (y_0 + \dot{y}_0)e^{-2t}$$

$$y_p(t) = e^{-t} - 5e^{-2t} + 5e^{-3t}$$

- (l) Consider the conventional approach of solving a differential equation as the sum of a homogeneous solution and a particular solution. For an input of the form $f(t) = e^{s_1 t} u(t)$, (e.g., $s_1 = -3$ in this example,) the particular solution is found to be $H(s_1) e^{s_1 t}$, where $H(s_1)$ is the value of $H(s)$ at $s = s_1$. Applying this to this example, we write the solution on the form:

$$y(t) = Ae^{-t} + Be^{-2t} + H(-3)e^{-3t}, \quad t \geq 0$$

By setting $t = 0+$, we obtain a relation between A, B . Another relation is obtained by differentiating with respect to t and then setting $t = 0+$. By solving these two equations for A, B show that $y(t)$ has the following form for $t \geq 0$:

$$y(t) = (2y(0+) + \dot{y}(0+) + 5)e^{-t} - (y(0+) + \dot{y}(0+) + 10)e^{-2t} + 5e^{-3t}$$

By applying the results of Eqs. (3), show that this solution is equivalent to that of Eq. (5).

- (m) Determine the observability matrix (and its inverse) for the second-order system of Eq. (4), that is,

$$F = \begin{bmatrix} C \\ CA \end{bmatrix}$$

$$\text{Answer: } F = \begin{bmatrix} -3 & -1 \\ 8 & 6 \end{bmatrix}, \quad F^{-1} = \frac{1}{10} \begin{bmatrix} -6 & -1 \\ 8 & 3 \end{bmatrix}.$$

- (n) For the state-space form of part (d), determine the initial state-vector $\mathbf{x}_0 = \mathbf{x}(0-) = \mathbf{x}(0+) = \mathbf{x}(0)$ by mapping the given initial conditions with the help of the observability matrix F , as discussed in class:

$$\begin{bmatrix} y_0 \\ \dot{y}_0 \end{bmatrix} = F\mathbf{x}_0 \quad \Rightarrow \quad \mathbf{x}_0 = F^{-1} \begin{bmatrix} y_0 \\ \dot{y}_0 \end{bmatrix}$$

$$\text{Answer: } \mathbf{x}_0 = \frac{1}{10} \begin{bmatrix} -6y_0 - \dot{y}_0 \\ 8y_0 + 3\dot{y}_0 \end{bmatrix}.$$

- (o) Using the state-transition matrix of part (g), calculate the homogeneous and forced parts of the state vector, that is,

$$\mathbf{x}(t) = \mathbf{x}_h(t) + \mathbf{x}_f(t) = e^{At}\mathbf{x}_0 + \int_0^t e^{A(t-\tau)} B f(\tau) d\tau$$

Answers:

$$\mathbf{x}_h(t) = e^{At}\mathbf{x}_0 = \frac{1}{10} \begin{bmatrix} 4(y_0 + \dot{y}_0)e^{-t} - 5(2y_0 + \dot{y}_0)e^{-2t} \\ 5(2y_0 + \dot{y}_0)e^{-t} - 2(y_0 + \dot{y}_0)e^{-2t} \end{bmatrix}$$

$$\mathbf{x}_f(t) = \int_0^t e^{A(t-\tau)} B f(\tau) d\tau = \frac{1}{2} \begin{bmatrix} 4e^{-2t} - e^{-t} - 3e^{-3t} \\ e^{-t} - 2e^{-2t} + e^{-3t} \end{bmatrix}$$

- (p) Calculate $y(t)$ using the state output equation:

$$y(t) = C\mathbf{x}(t) + Df(t)$$

and verify that it is again given by Eq. (5).

- (q) For the observer canonical form obtained in part (c), derive the corresponding $[A, B, C, D]$ state-space realization and write down the corresponding differential equations. Indicate on the block diagram exactly what signals are chosen to be the components of the state vector.
- (r) Consider the following state-space realization obtained by applying long-division to put $H(s)$ in the form,

$$H(s) = \frac{s^2 + 1}{s^2 + 3s + 2} = b_0 + \frac{A_1}{s + 1} + \frac{A_2}{s + 2} \quad (6)$$

and determine the values of the coefficients b_0, A_1, A_2 . By choosing appropriate internal states, derive the corresponding state-space parameters $[A, B, C, D]$ that represent Eq. (6) and write down the corresponding state equations. The state matrix A and transition matrix e^{At} are diagonal here. *Answers:*

$$A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \quad C = [2, -5], \quad D = 1$$

- (s) Carry out questions (m-o) for the diagonal realization of part (q). Verify that the resulting output is correctly given by Eq. (5).

Answers:

$$F = \begin{bmatrix} 2 & -5 \\ -2 & 10 \end{bmatrix}, \quad F^{-1} = \begin{bmatrix} 1 & 0.5 \\ 0.2 & 0.2 \end{bmatrix}, \quad \mathbf{x}_0 = \frac{1}{10} \begin{bmatrix} 5(2y_0 + \dot{y}_0) \\ 2(y_0 + \dot{y}_0) \end{bmatrix}$$

$$\mathbf{x}_f(t) = \frac{1}{2} \begin{bmatrix} e^{-t} - e^{-3t} \\ 2e^{-2t} - 2e^{-3t} \end{bmatrix}, \quad \mathbf{x}_h(t) = \frac{1}{10} \begin{bmatrix} 5(2y_0 + \dot{y}_0)e^{-t} \\ 2(y_0 + \dot{y}_0)e^{-2t} \end{bmatrix}$$

- (t) Write the decomposition of $H(s)$ given in part (b) as follows:

$$H(s) = b_0 + \frac{c_1 s + c_2}{s^2 + 3s + 2} = b_0 + \left(\frac{1}{s + 1} \right) \cdot \left(\frac{c_1 s + c_2}{s + 2} \right)$$

Draw block diagram realizations for the two factors,

$$\left(\frac{1}{s + 1} \right), \quad \left(\frac{c_1 s + c_2}{s + 2} \right)$$

and connect them in cascade (i.e., in series) and in parallel with the term b_0 to obtain a new block diagram realization of $H(s)$. Then, introduce appropriate internal states and derive the corresponding $[A, B, C, D]$ state-space representation. *Answers:* if the two factors are realized in their controller canonical forms,

$$A = \begin{bmatrix} -1 & 0 \\ 1 & -2 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad C = [-3, 5], \quad D = 1$$

(u) Determine the matrices $(sI - A)^{-1}$ and e^{At} of the previous part.
Answers:

$$\frac{1}{(s+1)(s+2)} \begin{bmatrix} s+2 & 0 \\ 1 & s+1 \end{bmatrix}, \quad \begin{bmatrix} e^{-t} & 0 \\ e^{-t} - e^{-2t} & e^{-2t} \end{bmatrix}$$

9. Repeat all questions (a-u) of the previous problem for the following system described by the transfer function:

$$H(s) = \frac{2s+1}{s^2+3s+2}$$

You will need to determine first the difference equation between input $f(t)$ and output $y(t)$. One simplification here is that $D = 0$ and the impulse response has no impulsive terms.